

Electromotive Force

Magnetic Flux $\Phi = \int_S \vec{B} \cdot d\vec{s}$



Flux is independent of the surface
prove

$$\int_V \text{div } \vec{B} d^3r = 0 \Rightarrow \int_{\partial V} \vec{B} \cdot d\vec{s} = 0$$

$$\Rightarrow \int_{S_1} \vec{B} \cdot d\vec{s} + \int_{S_2} \vec{B} \cdot d\vec{s} = 0$$

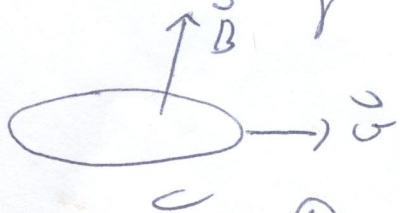
if we choose S_1 the normal in the same direction this gives

$$\int_{S_1} \vec{B} \cdot d\vec{s} - \int_{S_2} \vec{B} \cdot d\vec{s} = 0$$

An electromotive force occurs if a conductor moves through a magnetic field. The reason is that the electrons feel the Lorentz force

$$F_L = e \frac{\vec{v}}{c} \times \vec{B}$$

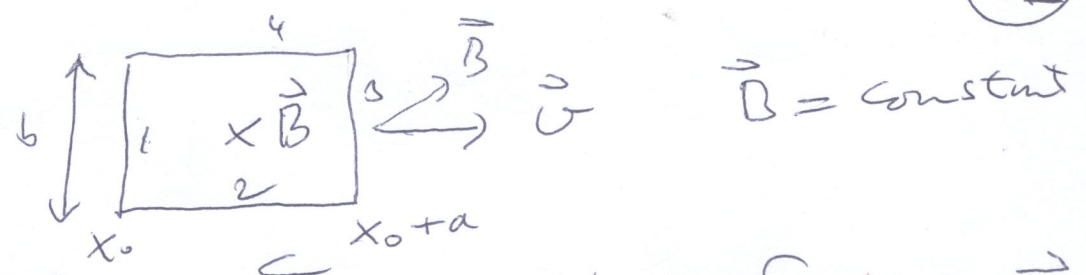
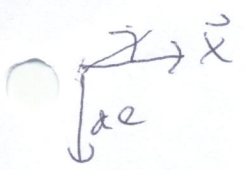
we can also interpret this as an effective electric field $\vec{E}_{\text{eff}} = \frac{\vec{v}}{c} \times \vec{B}$



Electromotive force

$$\mathcal{E}_{\text{eff}} = \oint_C \vec{E} \cdot d\vec{l} = \int \frac{\vec{v}}{c} \times \vec{B} \cdot d\vec{l}$$

Example



$$\frac{1}{c} \int_C \vec{v} \times \vec{B} \cdot d\vec{\ell} = \frac{1}{c} \frac{d}{dt} \int_C \vec{x} \times \vec{B} \cdot d\vec{\ell}$$

$$= \frac{1}{c} \frac{d}{dt} \int_C \vec{B} \cdot d\vec{\ell} \times \vec{x}$$

integral only nonzero on vertical sides

$$= \frac{1}{c} \frac{d}{dt} \left(\int_1 \vec{B} \cdot d\vec{\ell} \times \vec{x} + \int_3 \vec{B} \cdot d\vec{\ell} \times \vec{x} \right)$$

$$= \frac{1}{c} \frac{d}{dt} (B b x_0 - B b (x_0 + a))$$

$$= -\frac{1}{c} \frac{d}{dt} B A = -\frac{1}{c} \frac{d}{dt} \Phi$$

flux.

Next we will prove this in general

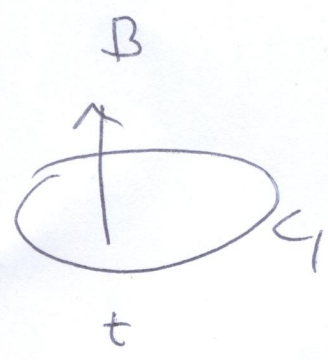
$$\mathcal{E}_{\text{eff}} = -\frac{1}{c} \frac{d\Phi}{dt}$$

the flux changes due to a moving circuit.

Faraday Law same formula but then the

changes due to the time dependence of the magnetic field.

flux $\phi = \int \vec{B} \cdot d\vec{s} = \int \vec{A} \cdot d\vec{\ell}$
" $\vec{\nabla} \times \vec{A}$



$C_2 = C_1 + \delta C_1$

$C_1: \vec{x}(\tau)$

$C_2: \vec{x}(\tau) + \delta \vec{x}(\tau)$

$x(0) = x(1)$

$0 \leq \tau < 1$

$d\vec{\ell} = \frac{d\vec{x}}{d\tau} d\tau$

$\delta\phi = \oint_{C_2} \vec{A} \cdot d\vec{\ell} - \oint_{C_1} \vec{A} \cdot d\vec{\ell}$

$= \int_0^1 d\tau A_i(x(\tau) + \delta x(\tau)) \frac{d(x_i + \delta x_i)}{d\tau}$

$- \int_0^1 d\tau A_i(x(\tau)) \cdot \frac{d x_i}{d\tau}$

$= \int_0^1 d\tau (\partial_k A_i(x)) \delta x_k \frac{d x_i}{d\tau} + A_i \frac{d(\delta x_i)}{d\tau}$

|| partial integration

$(-\frac{d}{d\tau} A_i)(\delta x_i)$

$= -\frac{d A_i}{d x_p} \frac{d x_p}{d\tau} \delta x_i$

$\Rightarrow \delta\phi = \int_0^1 d\tau (\partial_k A_i - \partial_i A_k) \delta x_k \frac{d x_i}{d\tau}$

$$d\vec{x} \frac{d\vec{x}}{d\tau} = d\vec{\ell}$$

(54)

$$\Rightarrow \delta\phi = \int_0^1 (d\vec{\ell})_q (\partial_\mu A_i - \partial_i A_\mu) \cdot \delta x_\mu$$

$$\text{Let us work out } (\delta \mathbf{x} \times \vec{\mathbf{B}})_i = (\delta \mathbf{x} \times (\vec{\nabla} \times \vec{\mathbf{A}}))_i$$

$$= \epsilon_{ijk} \delta x_j \epsilon_{kpq} \partial_{x_p} A_q$$

$$= (\delta_{ip} \delta_{jq} - \delta_{iq} \delta_{jp}) \delta x_j \partial_{x_p} A_q$$

$$= \delta x_q \partial_{x_i} A_q - \delta x_j \partial_{x_j} A_i$$

$$\text{So } \delta\phi = - \int_0^1 (\delta \mathbf{x} \times \vec{\mathbf{B}}) \cdot d\vec{\ell}$$

$$\Rightarrow -\frac{1}{c} \frac{\delta\phi}{\delta\tau} = + \frac{1}{c} \int_0^1 \left(\frac{d\vec{x}}{d\tau} \times \vec{\mathbf{B}} \right) \cdot d\vec{\ell}$$

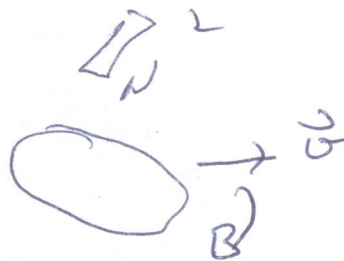
$$= \frac{1}{c} \int_0^1 \frac{\vec{v}}{c} \times \vec{\mathbf{B}} \cdot d\vec{\ell}$$

$$= \mathcal{E} \, dt$$

Faraday's law

move the magnet and keep the circuit

Fixed



Faraday's law

$$\mathcal{E} = - \frac{d\phi}{dt}$$

$$\oint \vec{E}_{\text{eff}} \cdot d\vec{e} = - \frac{d}{dt} \int \vec{B} \cdot d\vec{A}$$

|| stoke ||
$$\int \vec{\nabla} \times \vec{E} \cdot d\vec{A}$$

True for arbitrary loops

$$\Rightarrow \vec{\nabla} \times \vec{E} = - \frac{d}{dt} \vec{B}$$

differential form of Faraday's law.

~~59~~ ~~57~~ (60)



Magnetic energy

a magnetic field acting on a current transfers energy to the current.

The loss of energy ^{of the field} per second is given by

$$- \frac{dW}{dt} = \int d^3r \vec{E} \cdot \vec{j} = \int d^3r \vec{E} \cdot \frac{c}{4\pi} \vec{\nabla} \times \vec{H}$$
$$= \int d^3r \frac{c}{4\pi} \vec{H} \cdot \vec{\nabla} \times \vec{E}$$

$$= - \frac{c}{4\pi} \int d^3r \partial_t \vec{B} \cdot \vec{H}$$

$$B = \mu H$$
$$= - \frac{c}{4\pi} \partial_t \int d^3r (\vec{B} \cdot \vec{H})$$

$$\Rightarrow W = \frac{1}{4\pi} \int d^3r \vec{B} \cdot \vec{H}$$

$$dW = \sum_i q_i \vec{E}_i \cdot d\vec{s}$$

$$\frac{dW}{dt} = - \sum_i q_i \vec{E}_i \cdot \frac{d\vec{s}}{dt}$$

$$= - \int d^3r \vec{E}(r) \underbrace{\rho(r)}_j \underbrace{v(r)}_v$$

Galilean invariance Physics in frame A) and in frame B) is the same

$$Q = \int I dt = \int \frac{\mathcal{E}}{R} dt$$

Same amount of charge is transferred.

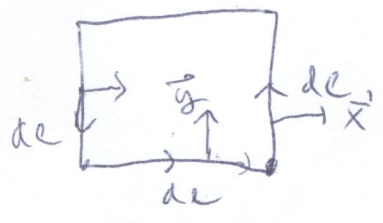
$$\Rightarrow \mathcal{E}_A = \mathcal{E}_B$$

Faraday's law

$$\mathcal{E} = - \frac{d\phi}{dt}$$

Paradox

$\vec{B} = \text{constant}$



$$\begin{aligned} \mathcal{E} &= \frac{1}{c} \oint \vec{v} \times \vec{B} \cdot d\vec{l} \\ &= \frac{1}{c} \oint \frac{d\vec{x}}{dt} \times \vec{B} \cdot d\vec{l} \\ &= \frac{1}{c} \oint d\vec{l} \times \frac{d\vec{x}}{dt} \cdot \vec{B} \\ &= \frac{d}{dt} \frac{1}{c} \oint d\vec{l} \times \vec{x} \cdot \vec{B} \end{aligned}$$

2 A
↑ wrong

solution on t.

the contour also depends

parameterization of C

$$x(\tau), 0 \leq \tau < 1$$

$$x(0) = x(1)$$

$$\mathcal{E} = \frac{1}{c} \int_0^1 d\tau \underbrace{\frac{d\vec{x}}{d\tau}}_{d\vec{e}} \times \frac{d\vec{x}}{d\tau} \cdot \vec{B}$$

$$= \frac{1}{c} \frac{d}{dt} \int_0^1 d\tau \frac{d\vec{x}}{d\tau} \times \vec{x} \cdot \vec{B} - \frac{1}{c} \int_0^1 d\tau \frac{d\dot{\vec{x}}}{d\tau} \times \vec{x} \cdot \vec{B}$$

$$\frac{1}{c} \int_0^1 d\tau \dot{\vec{x}} \times \frac{d\vec{x}}{d\tau} \cdot \vec{B}$$

$$= \frac{1}{c} \int_C \dot{\vec{v}} \times d\vec{e} \cdot \vec{B}$$

$$= \frac{1}{c} \int_C \dot{\vec{v}} \times \vec{B} \cdot d\vec{e}$$

$$\Rightarrow \frac{2}{c} \int_C \dot{\vec{v}} \times \vec{B} \cdot d\vec{e}$$

$$= \frac{1}{c} \frac{d}{dt} \int_0^1 d\tau \frac{d\vec{x}}{d\tau} \times \vec{x} \cdot \vec{B}$$

Maxwell equation

57

$$1) \vec{\nabla} \times \vec{E} = -\frac{1}{c} \partial_t B$$

$$2) \vec{\nabla} \cdot \vec{E} = 4\pi \rho$$

$$3) \vec{\nabla} \cdot \vec{B} = 0$$

$$4) \vec{\nabla} \times \vec{B} = \frac{4\pi}{c} \vec{j} + \frac{1}{c} \frac{\partial \vec{E}}{\partial t}$$

We will now argue that this term should be there

1) and 3) are consistent

$$\vec{\nabla} \cdot \vec{\nabla} \times \vec{E} = -\frac{1}{c} \partial_t \vec{\nabla} \cdot \vec{B} = 0$$

||
0

Continuity eq $\partial_t \rho + \vec{\nabla} \cdot \vec{j} = 0$

$$\partial_t \rho \neq 0 \Rightarrow \vec{\nabla} \cdot \vec{j} \neq 0$$

$$\text{and } \vec{\nabla} \cdot (\vec{\nabla} \times \vec{B}) = \frac{4\pi}{c} \vec{\nabla} \cdot \vec{j} \neq 0$$

||
0

Maxwell solved this by adding an extra term to 4

$$\vec{\nabla} \times \vec{B} = \frac{4\pi}{c} (\vec{j} + \vec{j}_0)$$

↑ displacement current

To be consistent, we need that

(5)

$$\vec{\nabla} \cdot (\vec{j} + \vec{j}_0) = 0$$

$$\Rightarrow \vec{\nabla} \cdot \vec{j}_0 = -\vec{\nabla} \cdot \vec{j} = +\frac{\partial \rho}{\partial t}$$

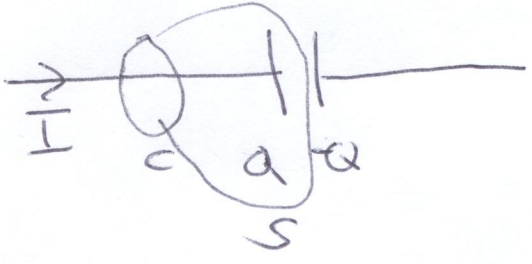
$$= \frac{1}{4\pi} \vec{\nabla} \cdot \frac{\partial \vec{E}}{\partial t}$$

$$\Rightarrow \vec{j}_0 = \frac{1}{4\pi} \frac{\partial \vec{E}}{\partial t} + \vec{\nabla} \times \vec{Q}$$

The simplest choice $\vec{Q} = 0$
appeared to be the right choice.

$$\Rightarrow \text{ME 4): } \vec{\nabla} \times \vec{B} = \frac{4\pi}{c} \vec{j} + \frac{1}{c} \frac{\partial \vec{E}}{\partial t}$$

Example of displacement current



$$\oint_C \vec{B} \cdot d\vec{l} = \frac{4\pi}{c} I$$

$$\int_S \vec{\nabla} \times \vec{B} \cdot d\vec{S}$$

choose S through capacitor.

~~which~~ without displacement current we have that $\vec{\nabla} \times \vec{B} = \frac{4\pi}{c} \vec{j} = 0$

with displacement current

$$\vec{\nabla} \times \vec{B} = \frac{4\pi}{c} \vec{j} + \frac{1}{c} \partial_t \vec{E}$$

$$\Rightarrow \int_S \vec{\nabla} \times \vec{B} \cdot d\vec{S} = \int_S \frac{1}{c} \partial_t \vec{E} \cdot d\vec{S}$$

$$= \frac{1}{c} \partial_t \int_S \vec{E} \cdot d\vec{S}$$

We can close S because $\vec{E} = 0$ inside C

$$= \frac{1}{c} \partial_t \int_V \underbrace{\text{div } \vec{E}}_{4\pi \rho} \cdot dV$$

$$= \frac{1}{c} 4\pi \partial_t Q = \frac{4\pi}{c} I \quad \underline{\text{okay}}$$

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$$= \int d^3r \frac{c}{4\pi} \vec{H} \cdot \vec{\nabla} \times \vec{E}$$

$$= -\frac{c}{4\pi} \int d^3r \partial_t \vec{B} \cdot \vec{H}$$

$$B = \mu H$$

$$= -\frac{c}{4\pi} \partial_t \int d^3r (\vec{B} \cdot \vec{H})$$

$$\Rightarrow W = \frac{1}{4\pi} \int d^3r \vec{B} \cdot \vec{H}$$

$$dW = \sum_i q_i \vec{E}_i \cdot d\vec{s}$$

$$\frac{dW}{dt} = -\sum_i q_i \vec{E}_i \cdot \frac{d\vec{s}}{dt}$$

$$= -\int d^3r \vec{E}(r) \underbrace{\rho(r)}_{\vec{j}}$$

(61)

We can rewrite this in terms of the vector potential.

$$W = \frac{1}{\mu_0} \int d^3r \vec{B} \cdot \vec{H} = \frac{1}{\mu_0} \int d^3r \vec{\nabla} \times \vec{A} \cdot \vec{H}$$

$$= \frac{1}{\mu_0} \int d^3r \epsilon_{ijk} \partial_j A_k \cdot H_i$$

$$= -\frac{1}{\mu_0} \int d^3r \epsilon_{ijk} A_k \partial_j H_i$$

$$= \frac{1}{\mu_0} \int d^3r \epsilon_{kji} A_k \partial_j H_i$$

$$= \frac{1}{\mu_0} \int d^3r A \cdot \underbrace{\vec{\nabla} \times \vec{H}}_{\frac{\mu_0}{c} \vec{j}}$$

$$W = \frac{1}{2c} \int d^3r \vec{A} \cdot \vec{j}$$

For a circuit this becomes $d^3r \vec{j} = I d\vec{\ell}$

$$W = \frac{1}{2c} \oint \vec{A} \cdot I d\vec{\ell}$$

$$= \frac{1}{2c} \int_S I \underbrace{\vec{\nabla} \times \vec{A}}_{\vec{B}} \cdot d\vec{A} = \frac{1}{2c} I \oint_{\text{flux}}$$

magnetic field depend linearly on the currents $\Rightarrow \Phi_i = c \sum_j \underbrace{L_{ij}}_{\text{coefficients of inductance}} I_j$

$$\Rightarrow W = \frac{1}{2} \sum I_i L_{ij} I_j$$

Momentum tensor

$$\vec{F} = \frac{1}{c} \int_V d^3r \vec{j} \times \vec{B}$$

$$\vec{j} = \sum_i q_i \vec{v}_i \delta(\vec{r} - \vec{r}_i)$$

↑
force
of field on current

$$\vec{\nabla} \times \vec{B} = \frac{4\pi}{c} \vec{j}$$

$$\Rightarrow F = \frac{1}{4\pi} \int_V d^3r \frac{(\vec{\nabla} \times \vec{B}) \times \vec{B}}{-\vec{B} \times (\vec{\nabla} \times \vec{B})}$$

$$F_k = \frac{1}{4\pi} \int_V d^3r B_i \partial_k B_i - B_i \partial_i B_k$$

$$= -\frac{1}{4\pi} \int_V d^3r \frac{1}{2} \partial_k \vec{B}^2 - \partial_i (B_i B_k)$$

note that $\partial_i B_i = 0$

$$= \frac{1}{4\pi} \int_V d^3r \partial_i (B_i B_k - \frac{1}{2} \delta_{ik} \vec{B}^2)$$

$$= \int_{\partial V} da n_i T_{ik}$$

momentum tensor $T_{ik} = \frac{1}{4\pi} (B_i B_k - \frac{1}{2} \delta_{ik} \vec{B}^2)$

Force on charges and current

$$\vec{F} = \int d^3r (\rho \vec{E} + \frac{1}{c} \vec{j} \times \vec{B})$$

$$\frac{1}{4\pi} \vec{\nabla} \cdot \vec{E} \quad \frac{1}{4\pi} (\vec{\nabla} \times \vec{B}) - \frac{1}{4\pi} \partial_t \vec{E}$$

$$\Rightarrow F_i = \frac{1}{4\pi} \int d^3r (E_i \partial_\mu E_\mu - \frac{1}{c} (\vec{E} \times \vec{B})_i + ((\vec{\nabla} \times \vec{B}) \times \vec{B})_i)$$

$$E_i \partial_\mu E_\mu = \partial_\mu (E_i E_\mu) + E_\mu \partial_i E_\mu - E_\mu \partial_\mu E_i - E_\mu \partial_i E_\mu$$

$$= \partial_\mu (E_i E_\mu - \frac{1}{2} \delta_{i\mu} \vec{E}^2) + E_\mu (\partial_i E_\mu - \partial_\mu E_i)$$

$$(\vec{E} \times (\vec{\nabla} \times \vec{E}))_i = E_\mu \epsilon_{ikp} \epsilon_{prs} \partial_r E_s$$

$$\stackrel{||}{=} -\frac{1}{2} \partial_t B = E_\mu \partial_i E_\mu - E \partial_\mu E_i$$

$$((\vec{\nabla} \times \vec{B}) \times \vec{B})_i = -\vec{B} \times (\vec{\nabla} \times \vec{B}) = -B_\mu \partial_i B_\mu + B_\mu \partial_\mu B_i$$

$$= \partial_\mu (B_\mu B_i - \frac{1}{2} \delta_{i\mu} \vec{B}^2)$$

$$\Rightarrow F_i = -\int \frac{d^3r}{4\pi c} \partial_t (\vec{E} \times \vec{B}) + \int d^3r \partial_\mu T_{i\mu}$$

$$T_{i\mu} = E_i E_\mu - \frac{1}{2} \delta_{i\mu} \vec{E}^2 + B_\mu B_i - \frac{1}{2} \delta_{i\mu} \vec{B}^2$$

$$\int_V d^3r \partial_\mu T_{i\mu} = \int_{\partial V} dS n_\mu T_{i\mu}$$

$$F_i = - \int \frac{d^3r}{4\pi c} \partial_t (\vec{E} \times \vec{B})_i + \int_{\partial V} ds n_k T_{ki}$$

//

$$\frac{d \vec{P}_{mech}}{dt} \qquad - \frac{d \vec{P}_{field}}{dt} \qquad \int_{\partial V} ds n_k T_{ki}$$

↑
momentum flow through surface

$$\Rightarrow \frac{d}{dt} (\vec{P}_{mechanical} + \vec{P}_{field}) = \int_{\partial V} ds n_k T_{ki}$$

⇒ momentum of the em field is

$$\vec{P} = \frac{1}{4\pi c} \int d^3r (\vec{E} \times \vec{B})$$

The angular momentum of the

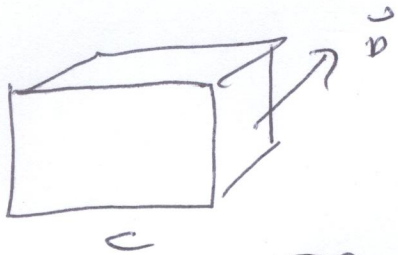
field is
$$\vec{L} = \frac{1}{4\pi c} \int d^3r \vec{r} \times (\vec{E} \times \vec{B})$$

Momentum density

693

60

$$\vec{p} = \frac{\vec{E} \times \vec{B}}{4\pi c}$$



Momentum flow per unit area per second is $c \cdot \vec{p} \cdot \vec{n} = \frac{\vec{E} \times \vec{B}}{4\pi} \cdot \vec{n}$

energy $E = pc$

\Rightarrow energy flow per second per unit area

is $\frac{\vec{E} \times \vec{B}}{4\pi} \cdot \vec{n}$

$\vec{p} = \frac{\vec{E} \times \vec{B}}{4\pi}$ is known as the

Poynting vector.