Electromagnetism 1

Torque on a cylinder

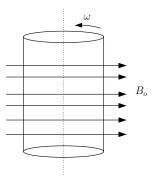
The constitutive relation is a relation between the macroscopic electrical current density in a medium and the applied fields. Recall that for a normal isotropic conductor *at rest* in an electric (*E*) and magnetic field (*B*) the constitutive relation in a linear response approximation is known as Ohm's law: $J = \sigma E$.

a) (2 points) For most materials, a symmetry principle forbids a generalized Ohm's law in the rest frame of the material of the form:

$$\boldsymbol{J} = \boldsymbol{\sigma} \boldsymbol{E} + \boldsymbol{\sigma}_{\boldsymbol{B}} \boldsymbol{B} \,. \tag{1}$$

Explain.

- b) (6 points) By making a Lorentz transformation for small velocities, deduce the familiar constitutive relation for a normal conductor *moving* non-relativistically with velocity u in an electric and magnetic field from the rest frame constitutive relation, Eq. ().
- c) (4 points) Now consider a solid conducting cylinder of radius *R* and conductivity σ rotating rather slowly with constant angular velocity ω in a uniform magnetic field *B*₀ perpendicular to the axis of the cylinder as shown below. Determine the current flowing in the cylinder.
- d) (8 points) Determine the torque required to maintain the cylinder's constant angular velocity. Assume that the skin depth is much larger than the radius of the cylinder.



Solution

- a) Parity forbids a constitutive relation including a magnetic field. Specifically, σ_B would have to be a pseudo-scalar, since J is a vector and B is a pseudo-vector. But, if the interactions of the medium are invariant under parity, and the ground state is parity symmetric, then medium expectation value of any pseudoscalar quantity is zero.
- b) In a frame where the conductor is at rest

$$\underline{J} = \sigma \underline{E} \tag{2}$$

the charge density $\rho = 0$. Make a Lorentz transformation from the conductor's rest frame to the lab frame, *i.e.* a frame moving with velocity -u relative to the conductor, so that the lab observer sees the conductor moving with velocity u. We have

$$J^{\mu} = \Lambda^{\mu}_{\ \nu} J^{\nu} \,. \tag{3}$$

Here the \underline{J} are the currents in the conductor frame, J are the currents in the lab frame.

To first order in *u* the Lorentz transformation matrix is

$$\Lambda^{\mu}_{\nu} = \begin{pmatrix} \gamma & \gamma u \\ \gamma u & \gamma \end{pmatrix} \approx \begin{pmatrix} 1 & u \\ u & 1 \end{pmatrix}$$
(4)

Thus

$$J \approx u \underbrace{\rho}_{=0} + \underline{I} = \sigma \underline{E}$$
⁽⁵⁾

We need to use the Lorentz transformation rule to relate \underline{E} to E and B.

The transformation rules for the *E* and *B* fields are

$$E_{\parallel} = \underline{E}_{\parallel} \tag{6}$$

$$B_{\parallel} = \underline{B}_{\parallel} \tag{7}$$

$$E_{\perp} = \gamma \underline{E}_{\perp} - \gamma \boldsymbol{u} / \boldsymbol{c} \times \underline{\boldsymbol{B}}$$
(8)

$$B_{\perp} = \gamma \underline{B}_{\perp} + \gamma \boldsymbol{u}/\boldsymbol{c} \times \underline{\boldsymbol{E}}$$
(9)

and the inverse results

$$\underline{E}_{\parallel} = E_{\parallel} \tag{10}$$

$$\underline{B}_{\parallel} = B_{\parallel} \tag{11}$$

$$\underline{E}_{\perp} = \gamma E_{\perp} + \gamma u/c \times B \approx E_{\perp} + u/c \times B$$
(12)

$$\underline{B}_{\perp} = \gamma B_{\perp} - \gamma \boldsymbol{u} / \boldsymbol{c} \times \boldsymbol{E} \tag{13}$$

So the constitutive relation becomes to first order

$$J = \sigma(E + \frac{u}{c} \times B) \tag{14}$$

Clearly the constitutive relation takes the form $J = \sigma f$ where f is the Lorentz force.

c) Using the result

$$\boldsymbol{J} = \boldsymbol{\sigma}(\boldsymbol{u}/\boldsymbol{c} \times \boldsymbol{B}_o) \,, \tag{15}$$

we find in cylindrical coordinates

$$J(\rho,\phi) = -\sigma \frac{\omega \rho B_o}{c} \cos \phi \hat{z} \,. \tag{16}$$

We see that the electrons (which carry negative charge) flow up the cylinder at $\phi = 0$ and down the cylinder at $\phi = \pi$.

d) The Lorentz force on the current induces a torque:

$$\tau = \int d^3 \mathbf{r} \, \mathbf{r} \times \left(\frac{\mathbf{J}}{c} \times \mathbf{B}_o\right) \,, \tag{17}$$

$$=L \int \rho d\rho d\phi \left[\frac{J}{c} (\mathbf{r} \cdot \mathbf{B}_o) - (\mathbf{r} \cdot \mathbf{J}/c) \mathbf{B}_o \right] , \qquad (18)$$

where L is the length of the cylinder. The second term in square braces integrates to zero while the first terms gives

$$\tau = L \int_0^R \rho d\rho \int d\phi \left[\left(-\sigma \frac{\omega \rho B_o}{c^2} \cos \phi \hat{z} \right) (\rho \cos \phi B_o) \right] , \qquad (19)$$

$$= -L\hat{z}\frac{\left(\pi\sigma\omega R^4 B_o^2\right)}{4c^2}\,.\tag{20}$$

This is the torque by the magnetic field on the cylinder. To maintain a constant angular velocity we need an external torque per unit length of

$$\frac{\tau}{L} = +\hat{z}\frac{\left(\pi\sigma\omega R^4 B_o^2\right)}{4c^2}\,.\tag{21}$$

Notes:

• An alternative way to derive this is to equate the work done per time by the external torque, $\tau \cdot \omega$, with the energy dissipation

$$\tau \cdot \omega = \int d^3 \mathbf{r} \frac{\mathbf{J} \cdot \mathbf{J}}{\sigma} \tag{22}$$

$$=L\frac{\sigma\omega^2}{4c^2}B_o^2\pi R^4 \tag{23}$$

• We next evaluate this numerically for copper. Expressing the torque in terms of the skin depth (which is taken from Wikipedia):

$$\delta = \sqrt{\frac{2c^2}{\sigma\omega}} = 6.5 \,\mathrm{cm}/\sqrt{f_{Hz}} \tag{24}$$

We find

$$\frac{\tau}{L} = \frac{R^4 B_o^2}{\delta^2} \frac{\pi}{2} \tag{25}$$

Converting to MKS and Tesla

$$B_o^2 \to \frac{B_o^2}{\mu_o} = 1 \frac{J}{m^3} 8 \times 10^5 \left(\frac{B_o}{\text{Tesla}}\right)^2 \tag{26}$$

So we find

$$\frac{\tau}{L} \approx 3 \,\mathrm{N} \left(\frac{R}{\mathrm{cm}}\right)^4 \left(\frac{f}{\mathrm{Hz}}\right) \left(\frac{B_o}{\mathrm{Tesla}}\right)^2 \qquad \text{with} \qquad R \ll \frac{6.5 \,\mathrm{cm}}{\sqrt{f \,\mathrm{in}\,\mathrm{Hz}}} \tag{27}$$

It is also interesting to calculate the current flowing through each hemi-cylinder of the wire.

$$\frac{I}{c} = \int \rho d\rho \int_{-\pi/2}^{\pi/2} d\phi J(\rho, \phi)/c$$
(28)

$$= -\frac{2}{3}\sigma \frac{\omega R^3 B_o}{c^2} \hat{z}$$
⁽²⁹⁾

$$= -\frac{4}{3} \frac{R^3 B_o}{\delta^2} \tag{30}$$

Or in MKS

$$\frac{I}{c} \to \sqrt{\mu_o} I \tag{31}$$

$$B \to \frac{B}{\sqrt{\mu_o}}$$
 (32)

which evaluates to a shockingly large current

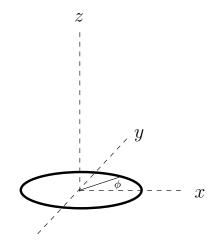
$$I = -\frac{4}{3} \frac{R^3 B_o}{\delta^2 \mu_o} \tag{33}$$

=310Amps
$$\left(\frac{f}{\text{Hz}}\right) \left(\frac{B}{\text{Tesla}}\right) \left(\frac{R}{\text{cm}}\right)^3$$
 (34)

Electromagnetism 2

Oscillating current on a ring

A current is driven through a ring of radius *R* in the *xy* plane (see below). Using complex notation, the current has a harmonic time dependence, $J(t, r) = e^{-i\omega t}J(r)$, and the spatial dependence is $J(r) = I_0 \sin(\phi) \,\delta(\rho - R) \delta(z) \hat{\phi}$.



- a) (4 points) Sketch the current flow at time t = 0 and $t = \pi/\omega$, and determine the charge density $\rho(t, \mathbf{r})$. Show that it corresponds to an oscillating electric dipole, and determine the electric dipole moment.
- b) In the long wavelength limit, and in the radiation zone, determine each of the following quantities in the *xz* plane at y = 0:
 - (a) (6 points) The vector potential A(t, r) in the Lorentz gauge.
 - (b) (4 points) The magnetic field B(t, r).
 - (c) (4 points) The (time averaged) angular distribution of the radiated power, $dP/d\Omega$.
- c) (2 points) What is the polarization of the radiated electric field when viewed along the *z* axis ?

Solution

We use Heavyside-Lorentz units.

a) Using current conservation, $\partial_t \rho + \nabla \cdot J = 0$ and a harmonic time dependence, $\rho(t, \mathbf{r}) = e^{-i\omega t}\rho(\mathbf{r})$,

$$-i\omega\rho(\mathbf{r}) = -\nabla \cdot \mathbf{J}(\mathbf{r}) = -\frac{1}{R}\frac{\partial}{\partial\phi}J^{\phi}.$$
 (1)

Thus

$$\rho(\mathbf{r}) = -\frac{I_0 \cos \phi}{-i\omega R} \delta(z) \delta(\rho - R)$$
⁽²⁾

Note, the charge distribution gives rise to a net dipole moment

$$\boldsymbol{p} = \int d^3 \boldsymbol{r} \rho(\boldsymbol{r}) \boldsymbol{r} = \frac{I_o R}{-i\omega} (-\pi \hat{\boldsymbol{x}})$$
(3)

pointed along the negative \hat{x} direction. If this is recognized then the remainder of this problem is just quoting the results of the electric dipole radiation.

b) a) In the dipole approximation we have

$$A(t, \mathbf{r}) = \frac{e^{-i\omega t + ikr}}{4\pi r} \int d^{3}\mathbf{r}' \mathbf{J}(\mathbf{r}')/c$$

= $\frac{e^{-i\omega t + ikr}}{4\pi r} \int \rho d\rho d\phi dz \,\hat{\boldsymbol{\phi}} \left(I_{0}/c\right) \sin \phi \,\delta(\rho - R)\delta(z) \,.$ (4)

With $\hat{\phi} = -\sin\phi \hat{x} + \cos\phi \hat{y}$ we obtain

$$\boldsymbol{A}(t,\boldsymbol{r}) = \frac{e^{-i\omega t + ikr}}{4\pi r} R(I_0/c)\pi(-\hat{\boldsymbol{x}}), \qquad (5)$$

$$= \frac{e^{-i\omega t + ikr}}{4\pi r} \frac{-i\omega}{c} p \tag{6}$$

b) Then

$$B = \nabla \times A, \qquad (7)$$

$$= n \times \frac{1}{c} \frac{\partial}{\partial t} A(t, \mathbf{r}), \qquad (8)$$

$$= \frac{e^{-i\omega t + ikr}}{4\pi r} (\mathbf{n} \times -\hat{\mathbf{x}})(-ikR)(I_0/c)$$
(9)

$$= \frac{e^{-i\omega t + ikr}}{4\pi r} \cos\theta(-\hat{y})(-ik\pi R)(I_0/c)$$
(10)

c) The radiated power is

$$\frac{dP}{d\Omega} = \frac{c}{2} \operatorname{Re}(r^2 \boldsymbol{n} \cdot (\boldsymbol{E} \times \boldsymbol{B}^*)).$$
(11)

With $E = -n \times B$, we have

$$\boldsymbol{n} \cdot (-\boldsymbol{n} \times \boldsymbol{B}) \times \boldsymbol{B}^* = |\boldsymbol{B}|^2, \qquad (12)$$

and

$$\frac{dP}{d\Omega} = \frac{c}{2}r^2|\boldsymbol{B}|^2 \tag{13}$$

$$= \frac{c}{32\pi^2} \cos^2\theta \left(\pi k R I_0 / c\right)^2 \tag{14}$$

It is perhaps useful to convert to MKS units:

$$\frac{I_0}{c} \rightarrow \sqrt{\mu_0} I \tag{15}$$

$$c \rightarrow \frac{1}{\sqrt{\mu_o \epsilon_o}}$$
 (16)

and using $\sqrt{\mu_o/\epsilon_o} = 376$ Ohm we find

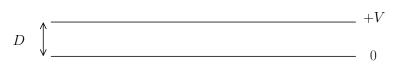
$$\frac{dP}{d\Omega} = 376 \,\text{Watts} \left(\frac{I_0}{\text{amps}}\right)^2 \frac{(kR)^2}{32} \cos^2\theta \tag{17}$$

c) Since the magnetic field is in the $-\hat{y}$ direction, for light propagating along the *z* axis the electric field is in the $-\hat{x}$ direction, *i.e.* along the direction of the dipole moment.

Electromagnetism 3

Parameters of an electron tube

Consider an idealized electron tube (diode) consisting of infinite planar cathode and anode separated by a distance D in the z direction (see below). The cathode (at z = 0) may be regarded as an infinite supply of free electrons at rest. The anode (at z = D) is at potential +V relative to the cathode. (V is sufficiently small that Newtonian physics applies.) The device is evacuated, so that only electrons are between the two electrodes. The current through such a device is determined by the flow of the charge of these electrons from the cathode (z = 0) to the anode (z = D).



- a) (10 points) Use Poisson's equation, the equation of continuity, and the conservation of energy to derive a differential equation for the electric potential $\Phi(z)$ in steady state. Make sure you have the sign correct, and state the boundary conditions explicitly.
- b) (6 points) Find $\Phi(z)$ and use it to determine the current density *J* as a function of the parameters of the problem and physical constants. *Hint:* Try a scaling solution of the form $\Phi(z) \propto z^{\beta}$.
- c) (4 points) Put in numbers for a centimeter-sized device and an anode potential of 300 volts to *estimate* the impedance typical of electron tube circuits.

Solution

a) Let v(z) = speed of electrons at distance *c* from the cathode.

Total energy of electron $= mv(z)^2/2 - e\Phi(z) = 0$, so $v(z) = (2e\Phi(z)/m)^{1/2}$.

Continuity: Current density $J = v(z)\rho(z)$ is constant, independent of z.

Poisson:
$$\nabla^2 \Phi = -\frac{\rho}{\epsilon_0}$$
 (1)

$$\frac{d^2\Phi}{dz^2} = +\frac{|J|}{\epsilon_0 v(z)} = \left[\frac{|J|}{\epsilon_0}\sqrt{\frac{m}{2e}}\right]\Phi(z)^{-1/2}.$$
 (2)

Boundary conditions are $\Phi(0) = 0$, $\Phi(D) = V$. Note that there is no boundary condition on $\frac{d\Phi}{dz}$ at z = 0.

b) Hypothesize a solution of the form $\Phi(z) = Az^{\beta}$.

$$\frac{d^2\Phi}{dz^2} = A\beta(\beta-1)z^{\beta-2} = KA^{-1/2}\beta^{-1/2}.$$
(3)

(Here *K* is the factor in square brackets in equation 2.)

This works if $\beta - 2 = -1/2$, *i.e.*, $\beta = 4/3$ and $\frac{4}{9}A^{3/2} = K$. The solution is

$$\Phi(z) = \left(\frac{9J}{4\epsilon_0}\right)^{2/3} \left(\frac{m}{2e}\right)^{1/3} z^{4/3}.$$
 (4)

The boundary condition that $\Phi(D) = V$ leads to

$$|J| = \frac{4\epsilon_0}{9} \sqrt{\frac{2e}{m}} \frac{V^{3/2}}{D^2}.$$
(5)

c) To substitute units, insert a factor of $c = 1/\sqrt{\mu_0 \epsilon_0}$, note that

$$m_e c^2 = 0.5 \, {
m MeV} = 0.5 imes 10^6 \, {
m eV}$$
 ,

and recall that $\sqrt{\mu_o/\epsilon_o} = 376 \,\Omega$. We find (using $(e \cdot V = 300 \,\text{eV})$)

$$|J| = \frac{4}{9} \left(\frac{V}{376 \,\Omega}\right) \frac{1}{D^2} \sqrt{\frac{2e \cdot V}{mc^2}} \tag{6}$$

$$= 121 \frac{\text{Amps}}{\text{meter}^2} \left(\frac{V}{300 \text{ Volts}}\right)^{3/2} \left(\frac{\text{cm}}{D}\right)^2 \tag{7}$$

So taking the plate area to be 1 cm^2

$$\frac{V}{I} = 1.59 \times 376 \,\Omega \,\sqrt{\frac{mc^2}{e \cdot V}} \frac{D^2}{\text{Area}} \tag{8}$$

$$= 25000 \,\Omega \sqrt{\frac{300 \,\text{Volts}}{V}} \left(\frac{D^2/\text{Area}}{1}\right) \tag{9}$$